

I. Concepts and Tools

- Mathematics for Dynamic Systems
 - Differential Equation
 - Transfer Function
 - State Space
- Time Response
 - Transient
 - Steady State
- Frequency Response
 - Bode and Nyquist Plots
 - Stability and Stability Margins
- Extensions to Digital Control

A Differential Equation of Motion

- Newton's Law:

$$\ddot{y}(t) = f(t, y(t), \dot{y}(t), w(t)) + bu(t)$$

- A Linear Approximation:

$$\ddot{y}(t) = -\frac{\mu}{J} \dot{y}(t) + w(t) + \frac{K_T}{J} u(t)$$

Laplace Transform and Transfer Function

$$Y(s) = \int_0^{\infty} y(t)e^{-st} dt$$

$$\ddot{y}(t) = -\frac{\mu}{J} \dot{y}(t) + \frac{K_T}{J} u(t)$$

⇓

$$s^2 Y(s) = \left(-\frac{\mu}{J}\right) s Y(s) + \frac{K_T}{J} U(s)$$

⇓

$$\frac{Y(s)}{U(s)} = G_p(s) = \frac{K_T}{s(Js + \mu)}$$

State Space Description

$$\ddot{y}(t) = -\frac{\mu}{J} \dot{y}(t) + \frac{K_T}{J} u(t)$$

\Downarrow

$$x_1 = y, x_2 = \dot{y}$$

\Downarrow

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & -\frac{\mu}{J} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{K_T}{J} \end{bmatrix} u$$

$$y = [1 \quad 0] \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$\text{Let } x = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$\begin{cases} \dot{x} = Ax + Bu \\ y = Cx + Du \end{cases}$$

with

$$A = \begin{bmatrix} 0 & 1 \\ 0 & -\frac{\mu}{J} \end{bmatrix}, B = \begin{bmatrix} 0 \\ \frac{K_T}{J} \end{bmatrix}$$

$$C = [1 \quad 0], D=0$$

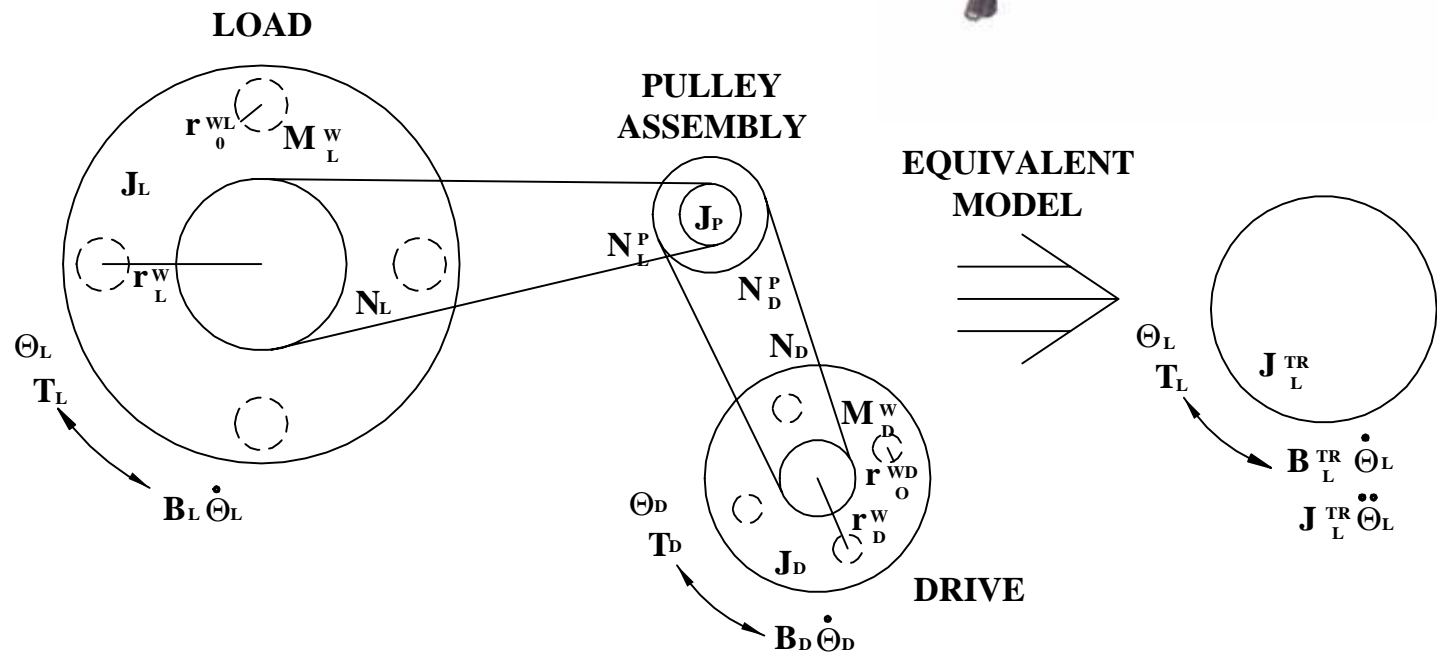
From State Space to Transfer Function

$$\begin{aligned} G_p(s) &= C(sI - A)^{-1}B + D \\ &= \frac{K_T}{s(Js + \mu)} \end{aligned}$$

Linear System Concepts

- States form a linear vector space
- Controllable Subspace and Controllability
- Observable Subspace and Observability
- The Linear Time Invariance (LTI) Assumptions
- Stability
 - Lyapunov Stability (for linear or nonlinear systems)
 - LTI System Stability: poles/eigenvalues in RHP

A Motion Control Problem



From Differential Eq. To Transfer Function

$$T_L = J_T \cdot \ddot{\Theta} + B_T \cdot \dot{\Theta}$$

$$T_L = T_D \cdot g r_T$$

$$TF = \frac{\Theta_L}{T_D} = \frac{g r_T}{s(J_T \cdot s + B_T)}$$

$$T_D = v_{CS} \cdot K_S \cdot K_A \cdot K_T$$

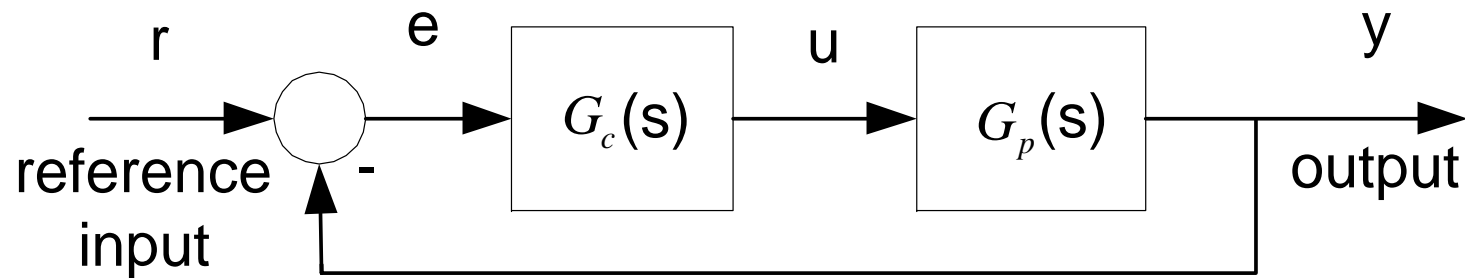
$$G_p(s) = \frac{\Theta_L}{v_{CS}} = \frac{K_S \cdot K_A \cdot K_T \cdot g r_T}{s(J_T \cdot s + B_T)}$$

Transfer Function model of the motion plant

$$G_p(s) = \frac{K_S \cdot K_A \cdot K_T \cdot gr_T}{s(J_T \cdot s + B_T)}$$

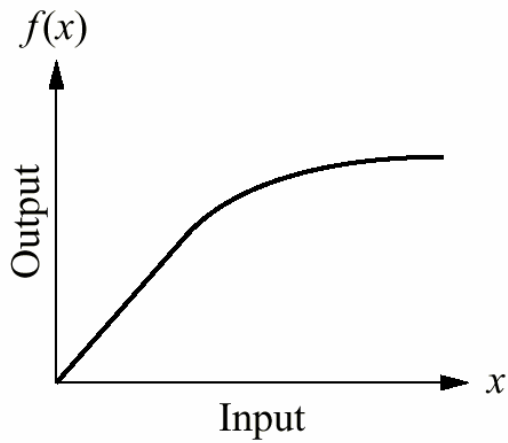
$$G_p(s) = \frac{K}{s(Js + \alpha)}$$

Unity Feedback Control System

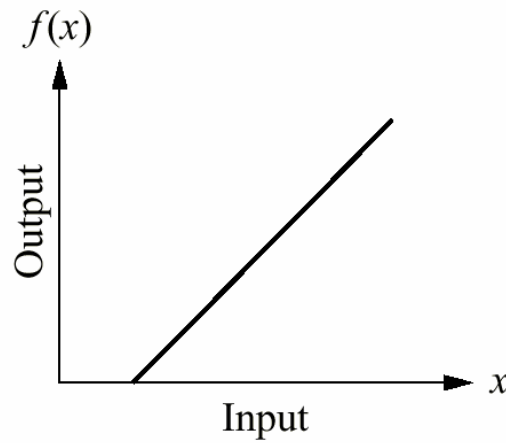


Common Nonlinearities

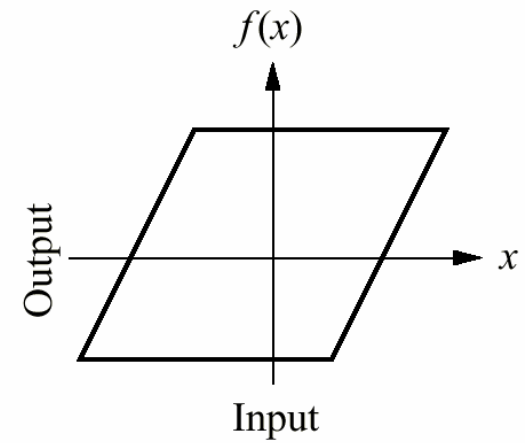
Amplifier saturation



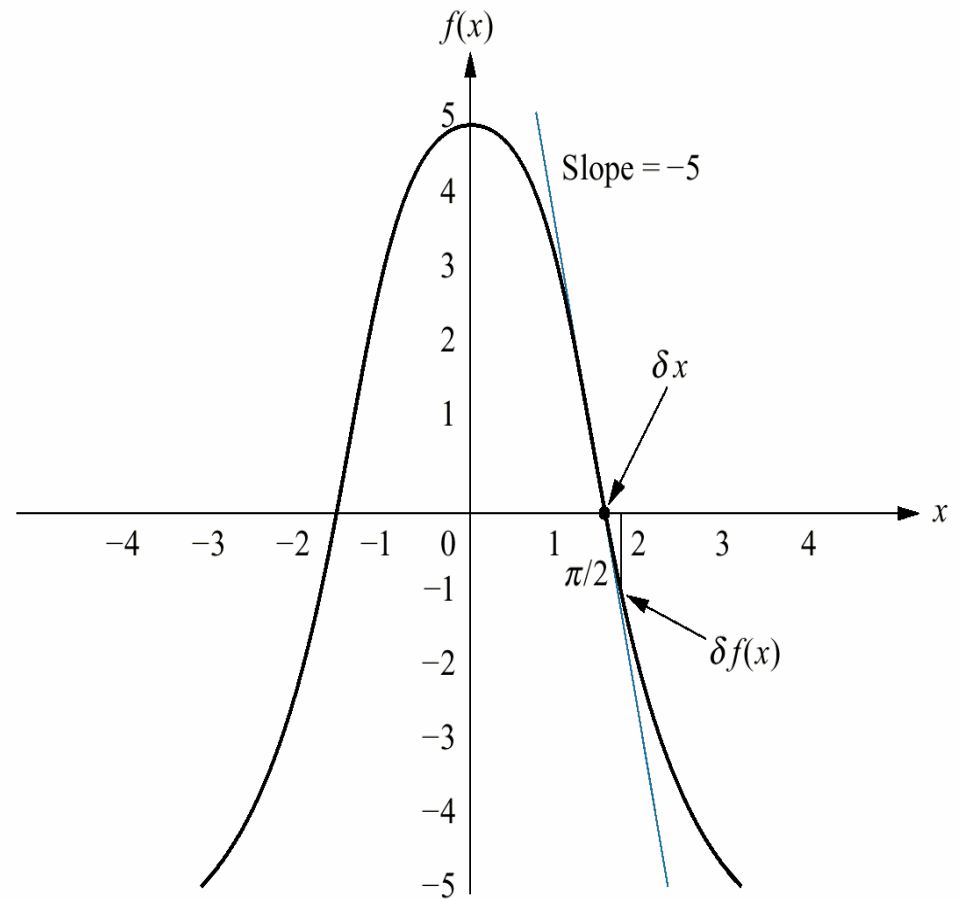
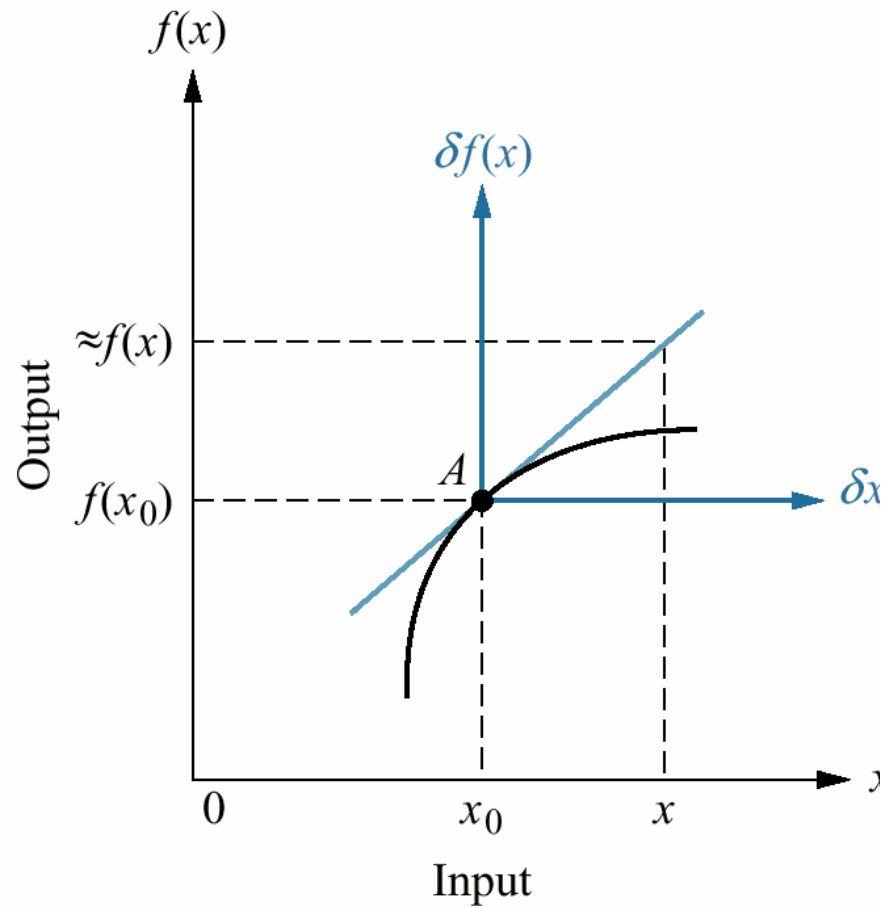
Motor dead zone



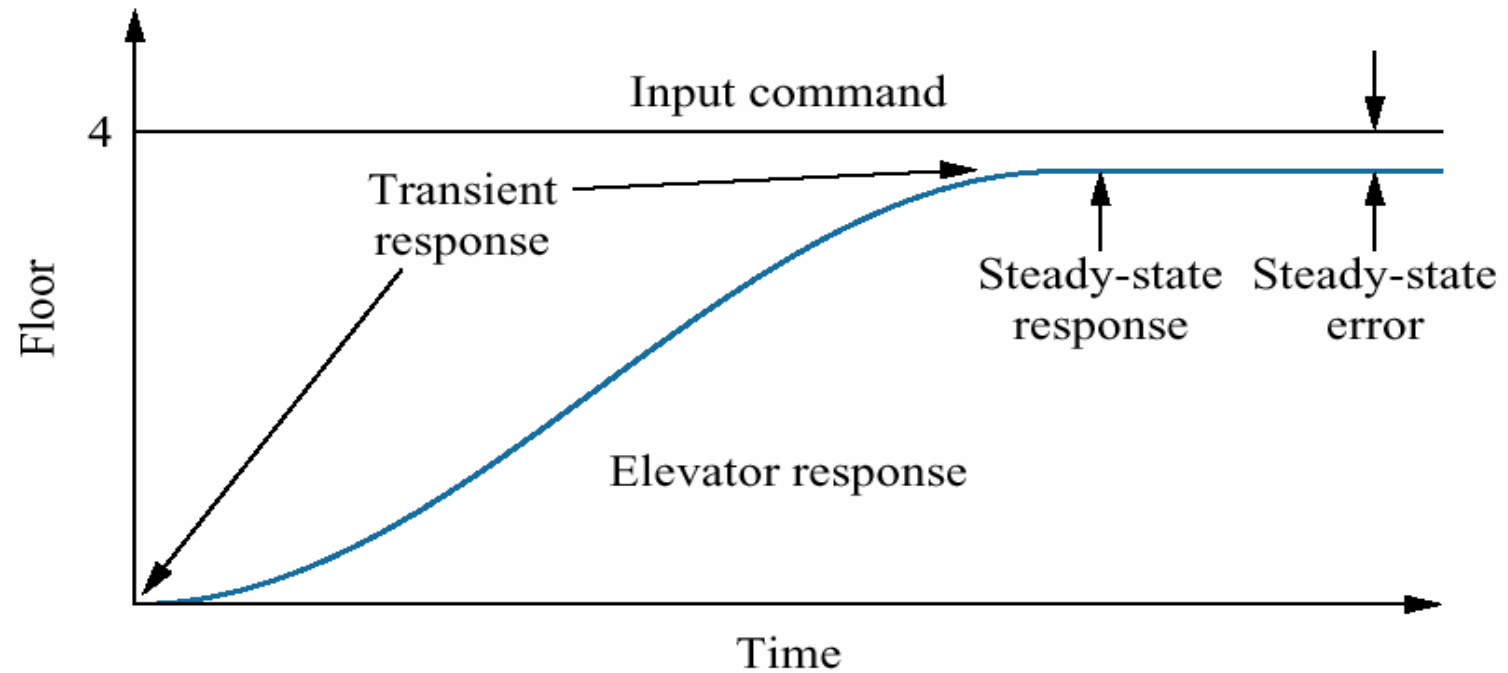
Backlash in gears



Linearization

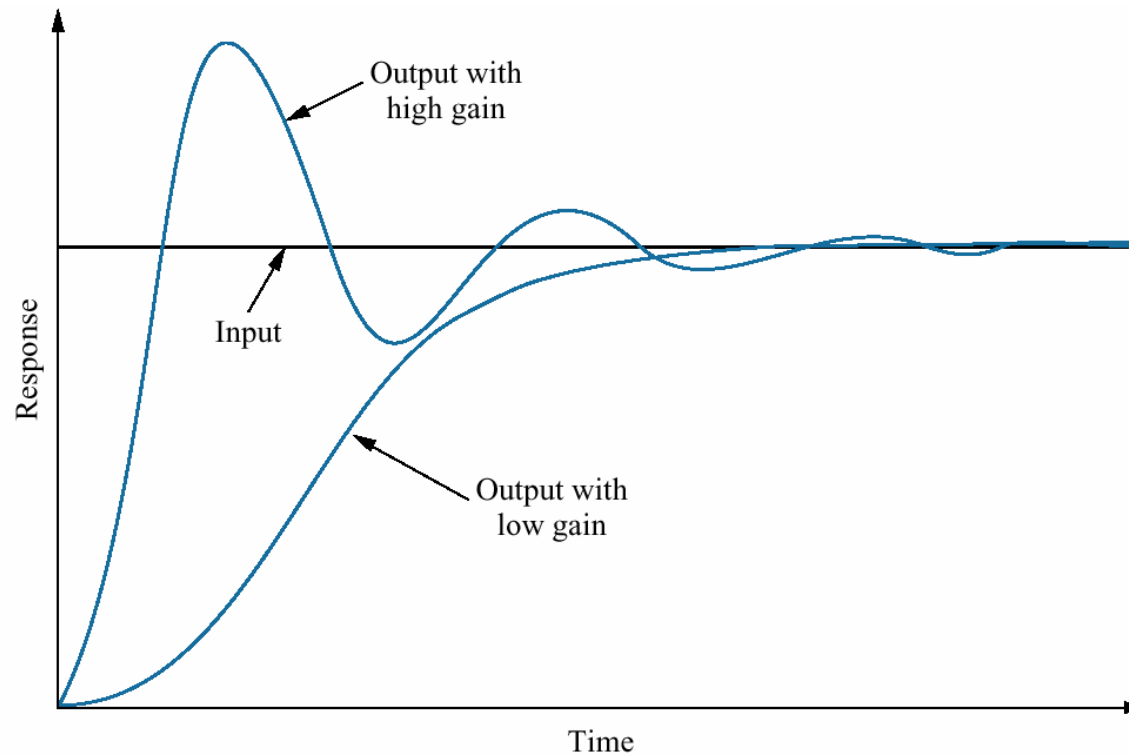


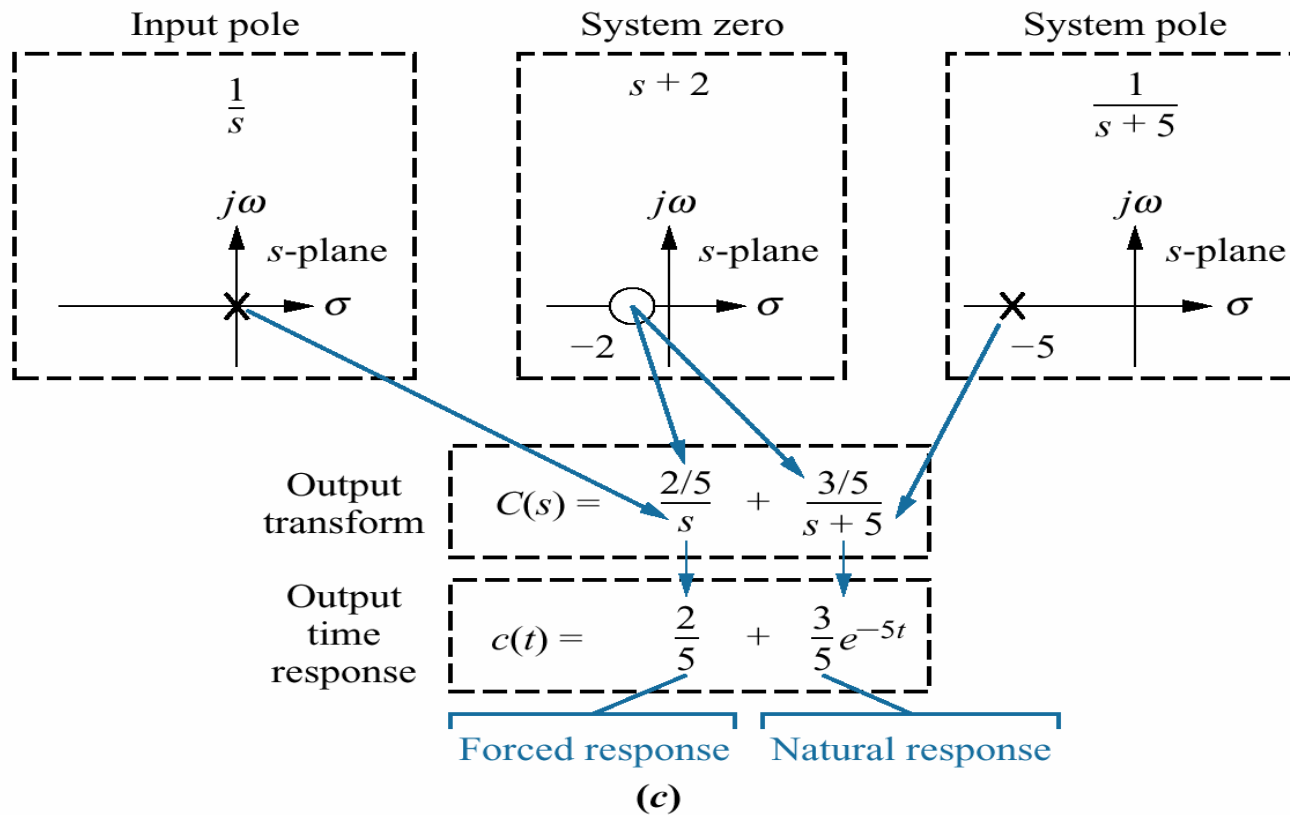
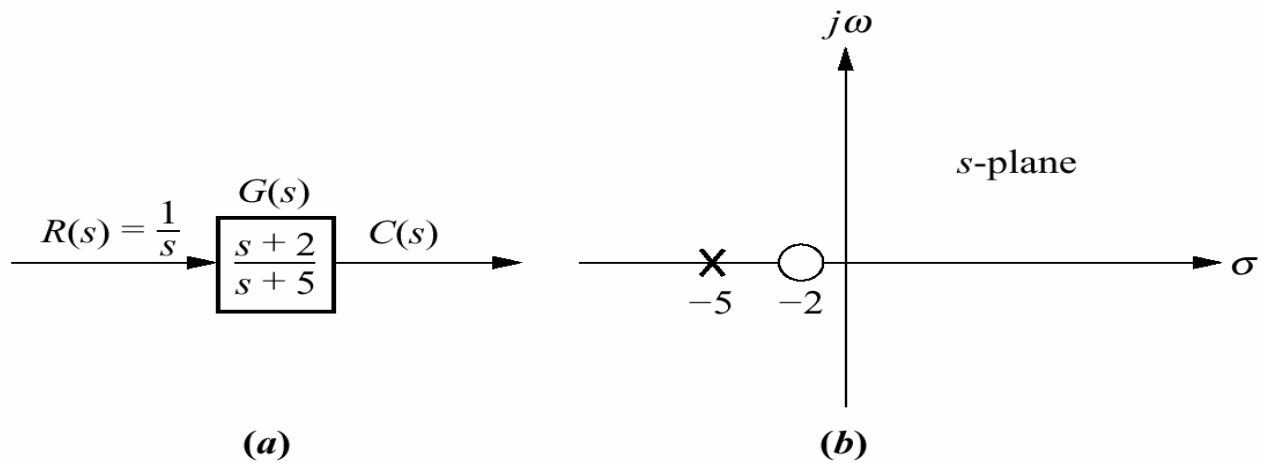
Time Response



Open Loop Transient Response

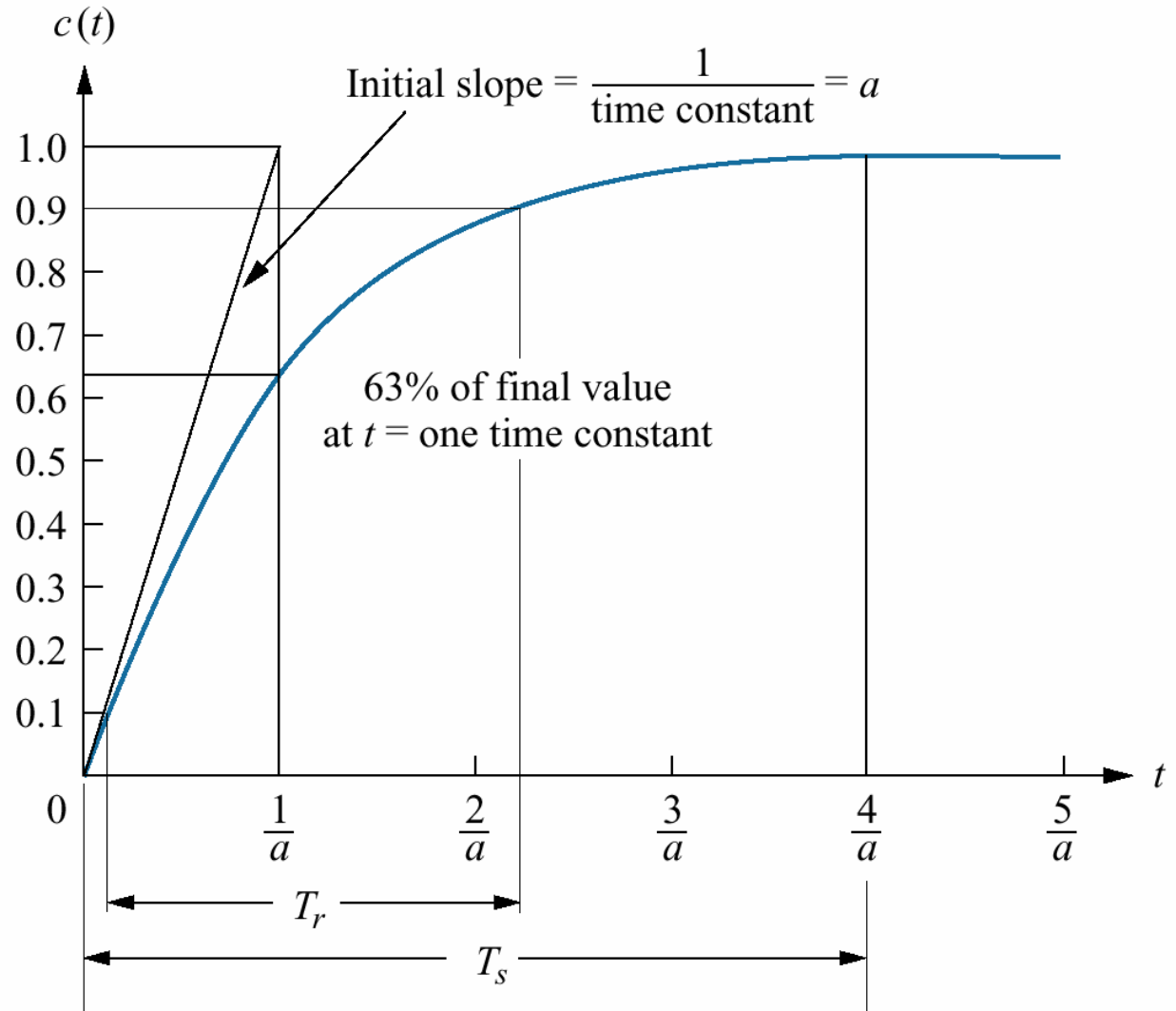
- How parameters of transfer functions affect output
- Terminologies for 1st and 2nd order systems





First Order Transfer Function

$$G(s) = \frac{a}{(s + a)}$$
$$= \frac{1}{(\tau s + 1)}$$



Pure 2nd Order Transfer Functions

$$G(s) = \frac{1}{\left(\frac{s}{\omega_n}\right)^2 + 2\xi\left(\frac{s}{\omega_n}\right) + 1}$$

ξ : damping ratio, ω_n : natural frequency

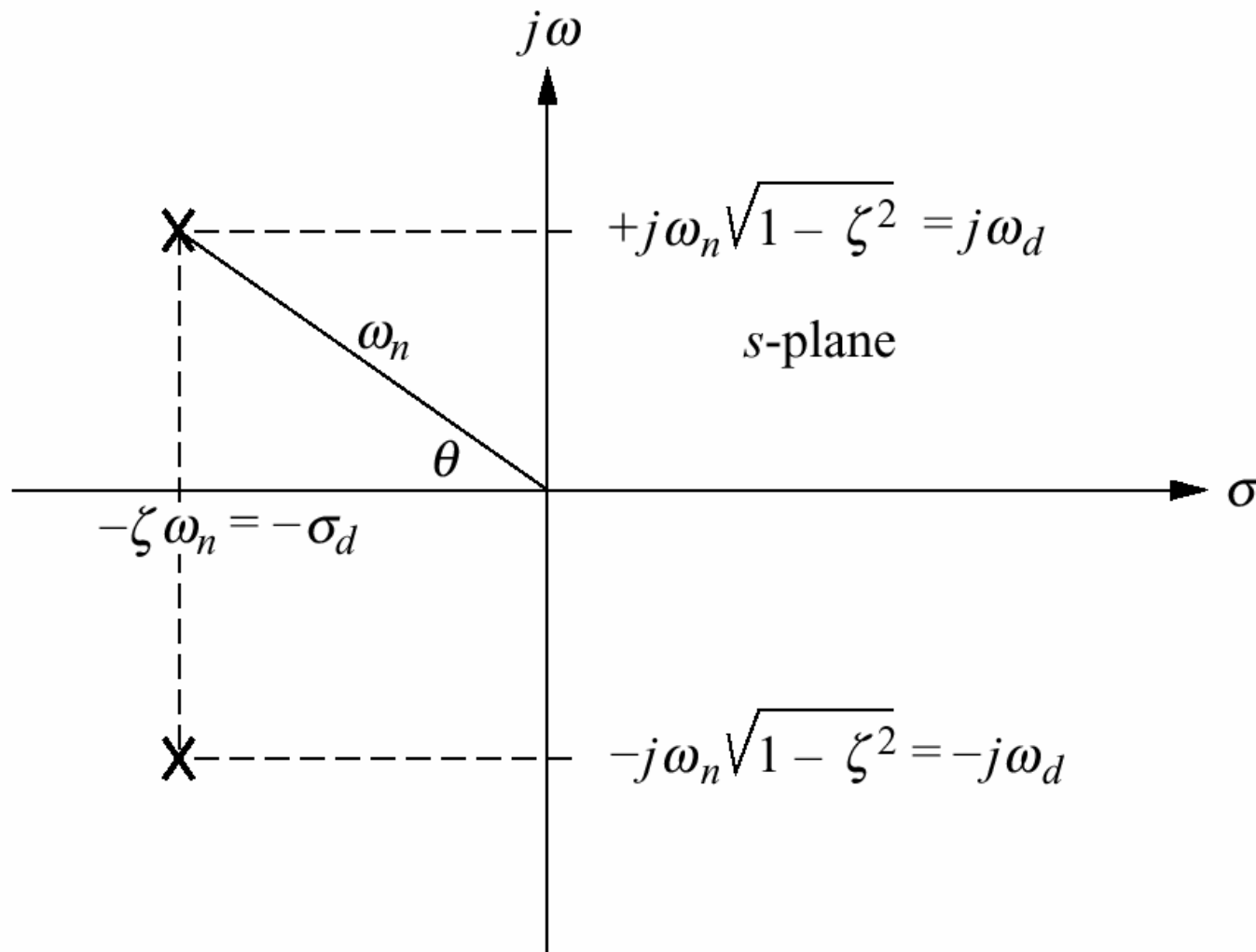
$\xi > 1$: overdamped

$\xi < 1$: underdamped

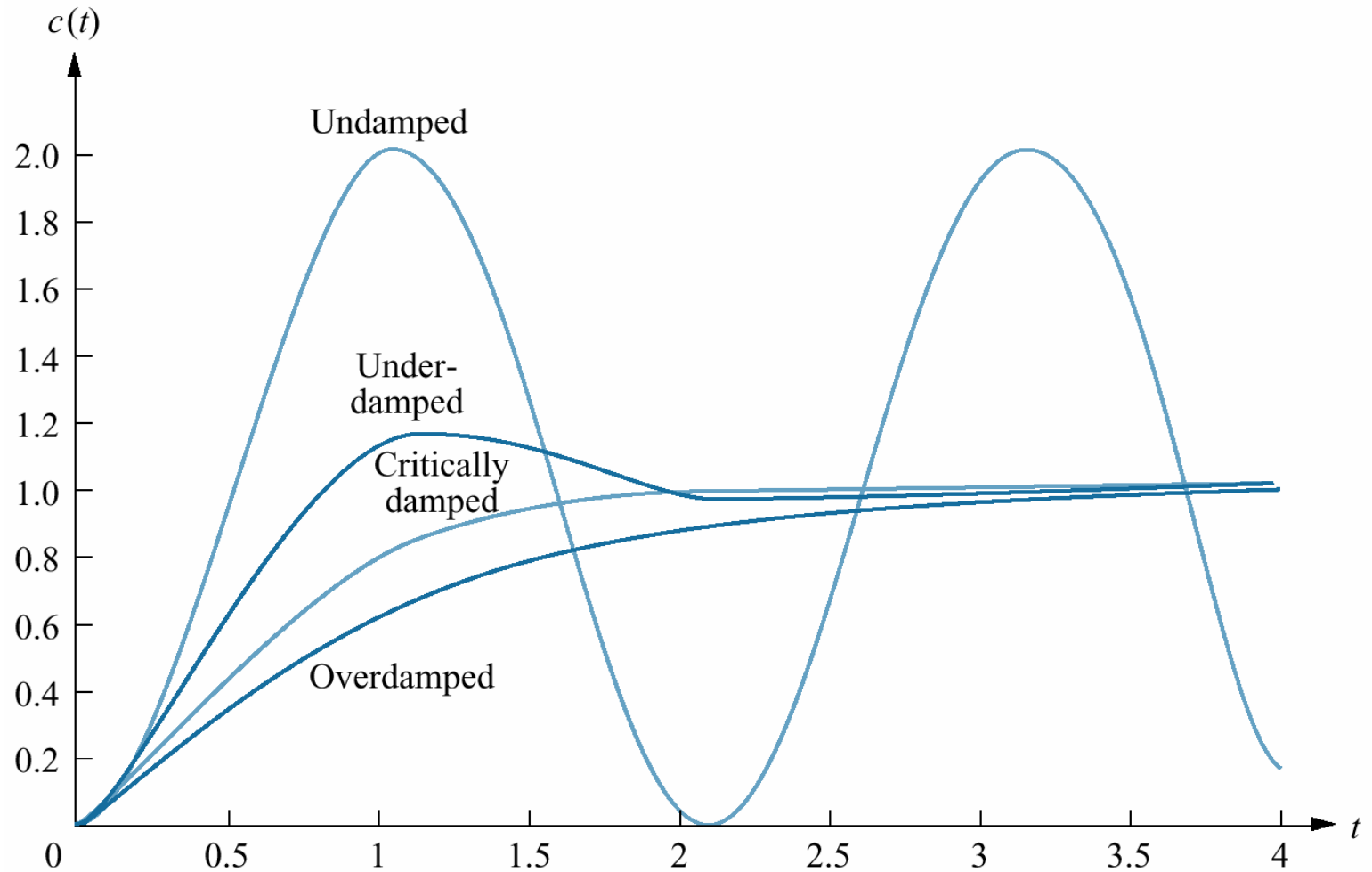
$\xi = 1$: critically damped

$\xi = 0$: undamped

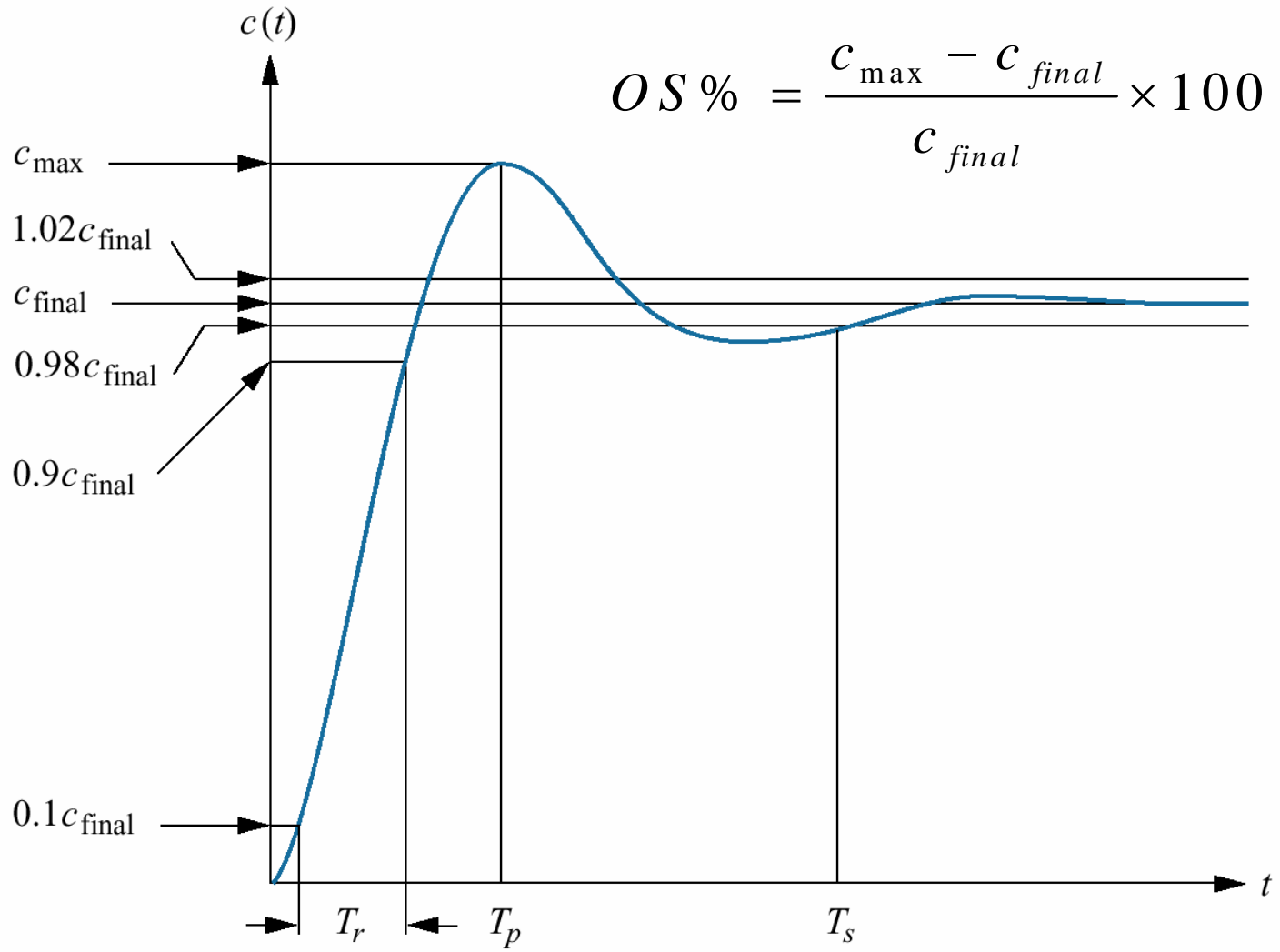
Pure 2nd Order Transfer Functions



Pure 2nd Order Transfer Functions



Terminologies

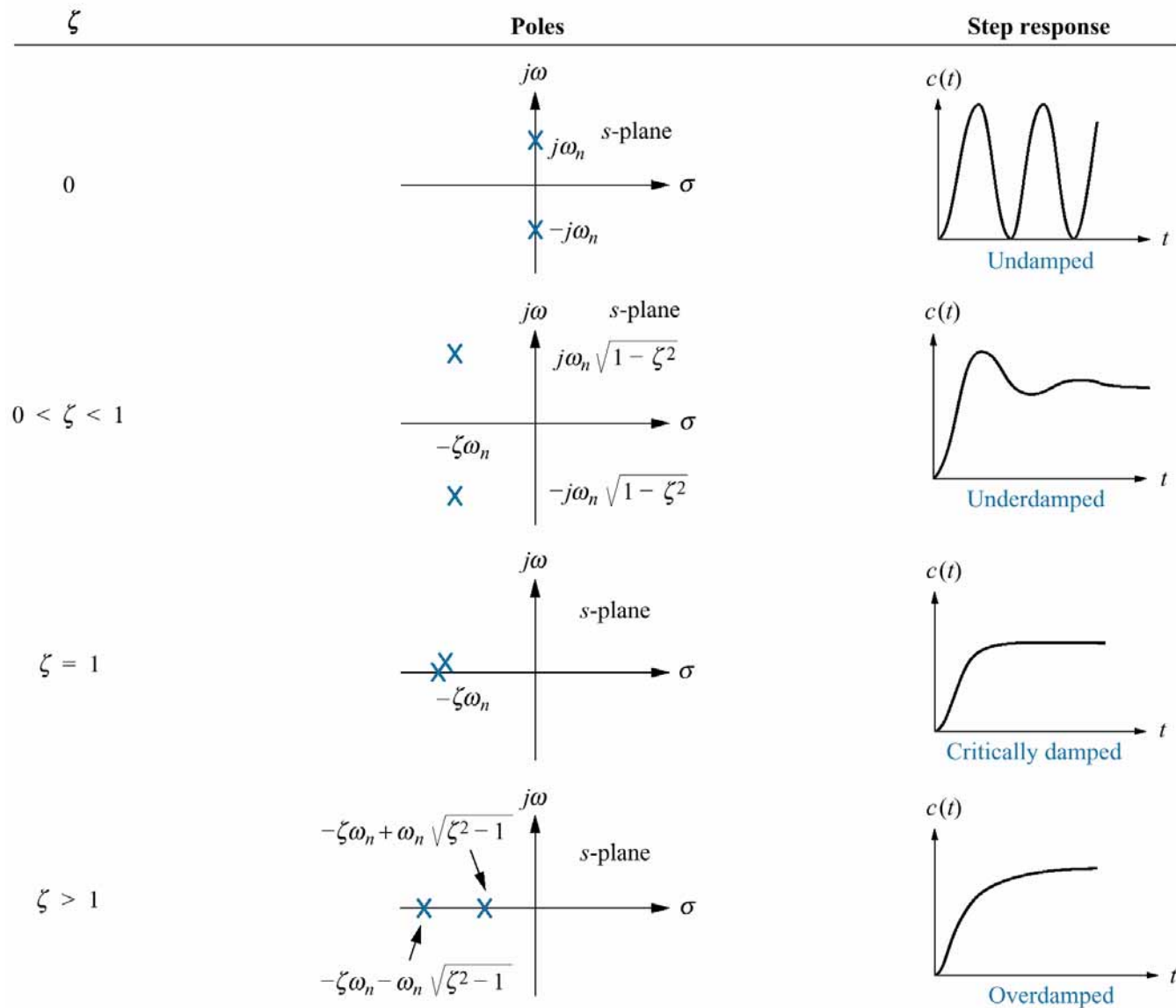


Calculations

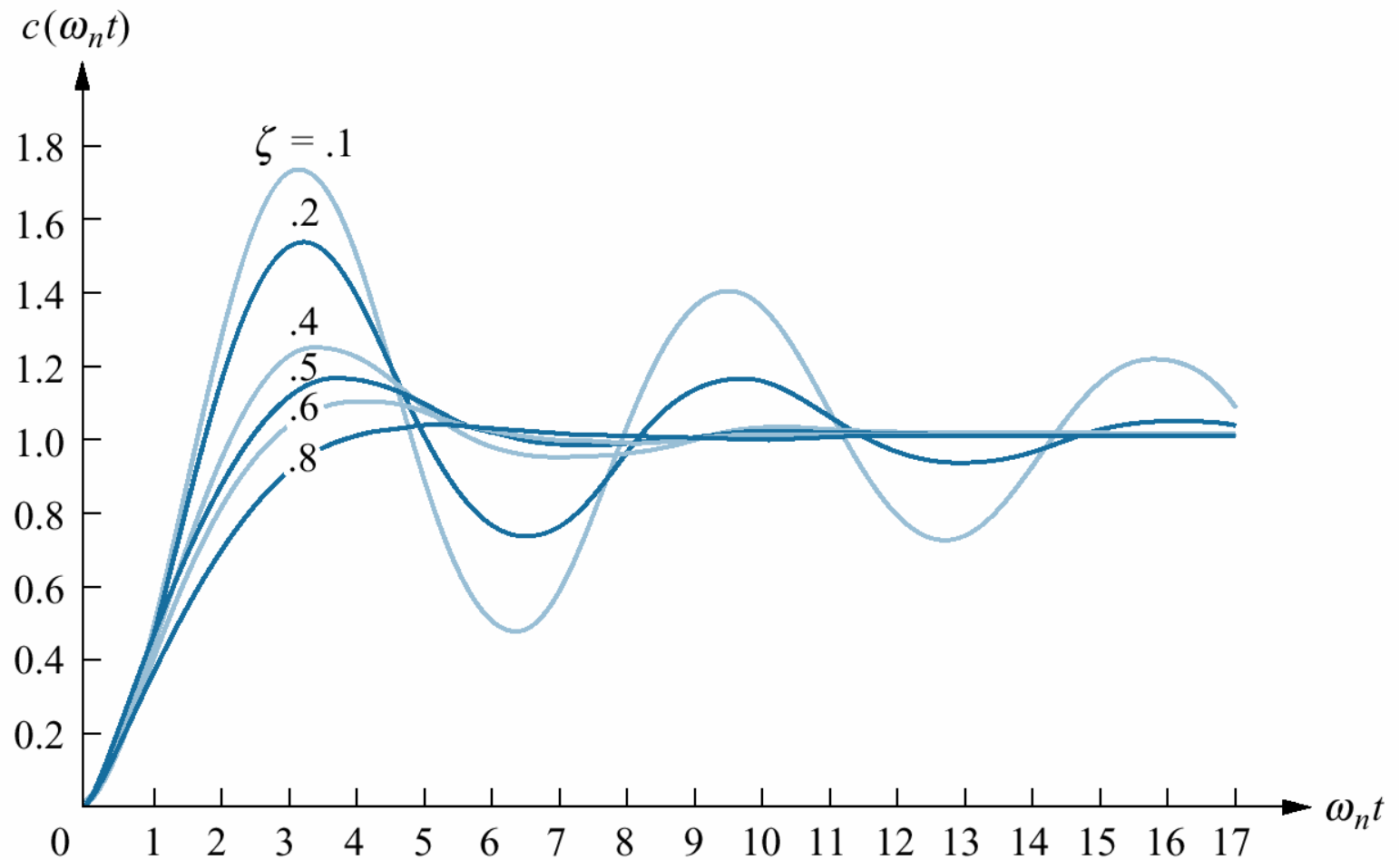
$$OS\% = e^{-(\xi\pi/\sqrt{1-\xi^2})} \times 100$$

$$T_s = \frac{4}{\xi\omega_n}$$

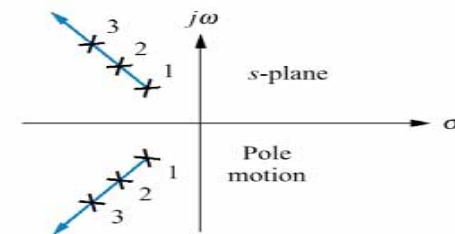
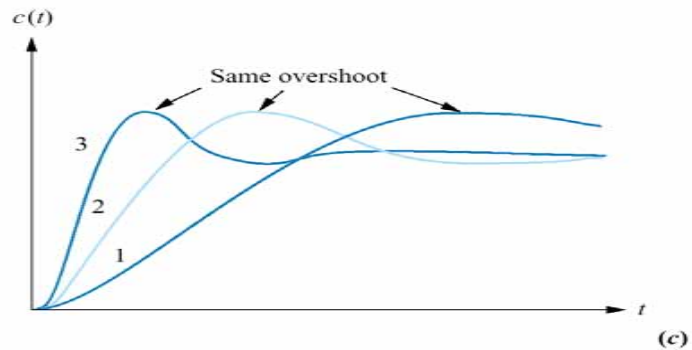
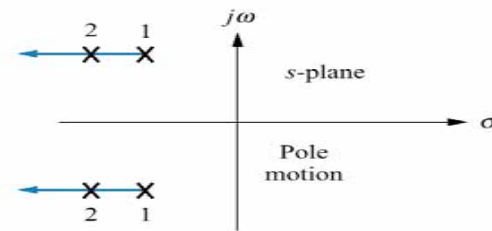
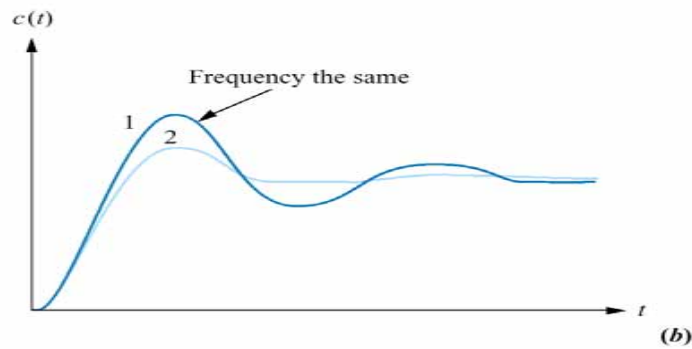
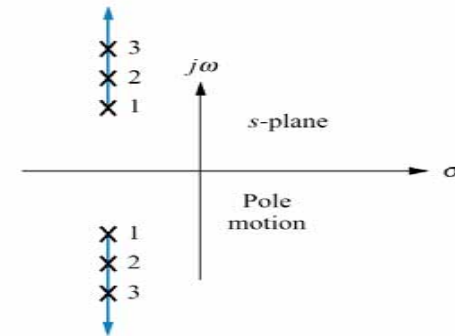
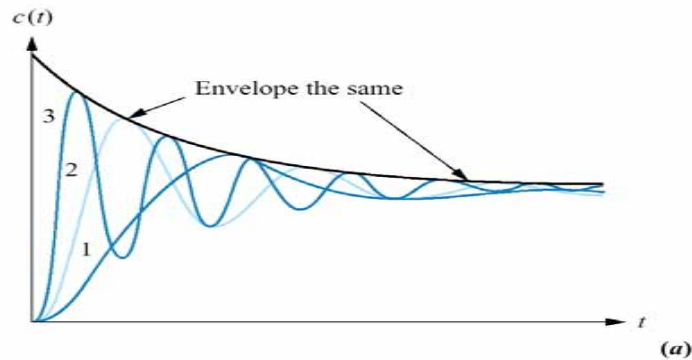
Pure 2nd Order Transfer Functions



Pure 2nd Order Transfer Functions



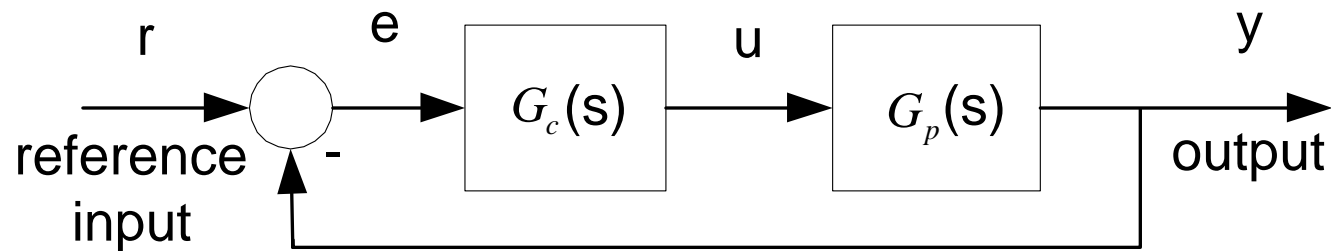
Pure 2nd Order Transfer Functions



Steady State Response

Steady state response is determined by the dc gain: $G(0)$

Steady State Error



$$e_{ss} = e(t) \Big|_{t \rightarrow \infty} = sE(s) \Big|_{s \rightarrow 0}$$

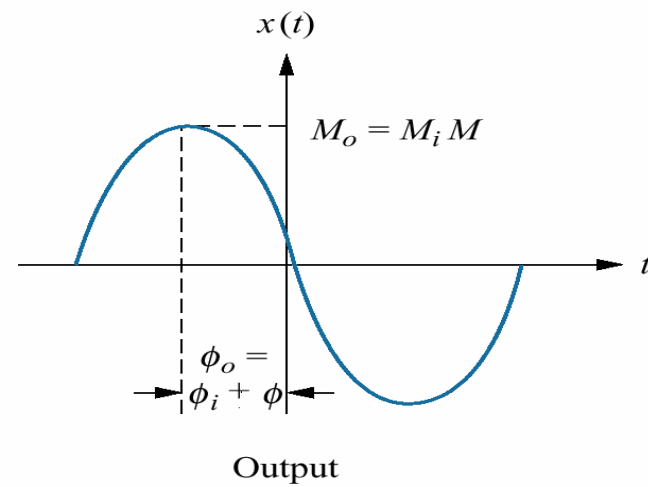
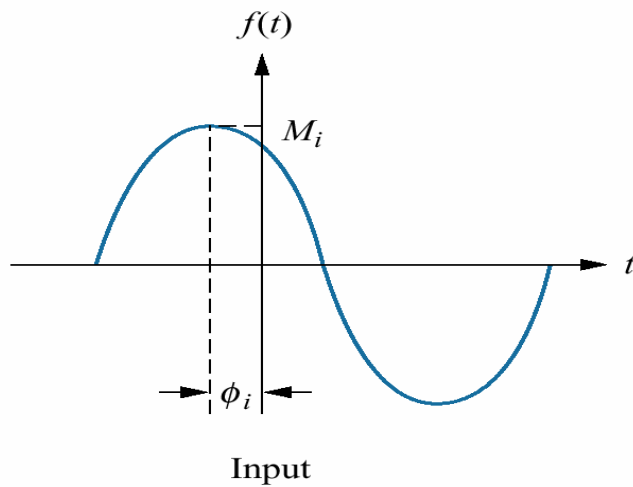
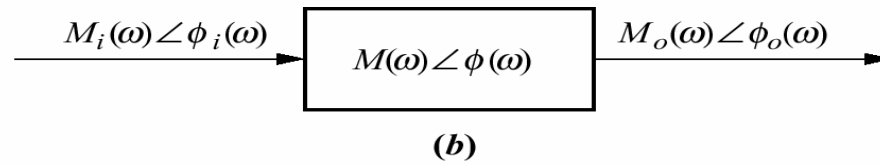
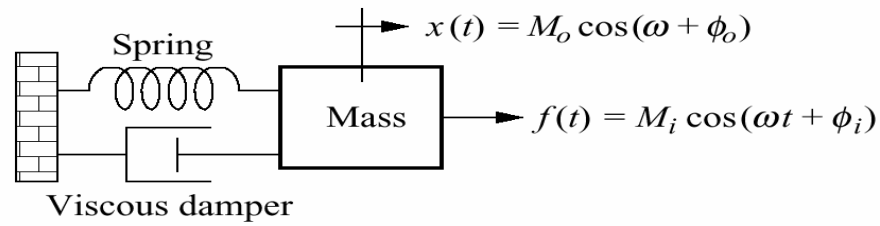
$$E(s) = \frac{R(s)}{1 + G_c(s)G_p(s)}$$

Frequency Response:

The MOST useful concept in control theory

- Performance Measures
 - Bandwidth
 - Disturbance Rejection
 - Noise Sensitivity
- Stability
 - Yes or No?
 - Stability Margins (closeness to instability)
 - Robustness (generalized stability margins)

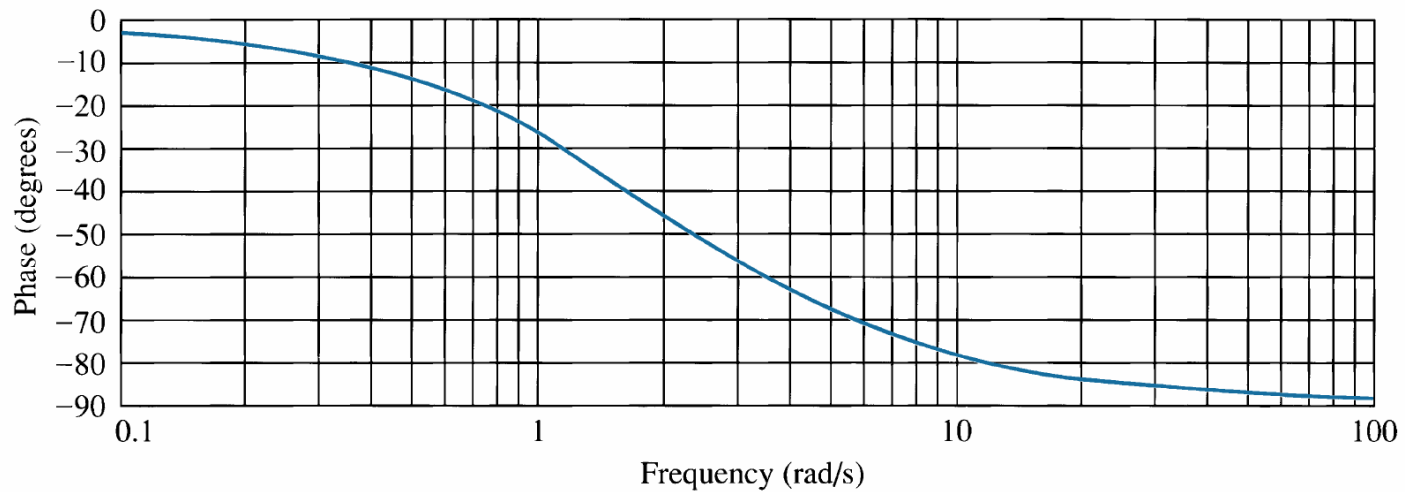
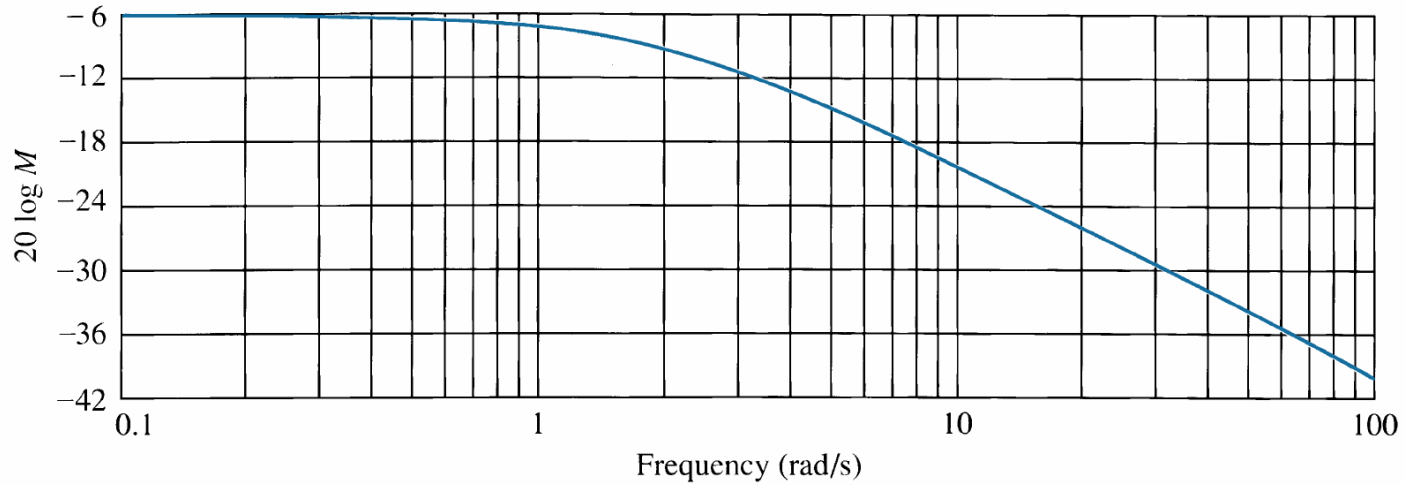
Frequency Response



(c)

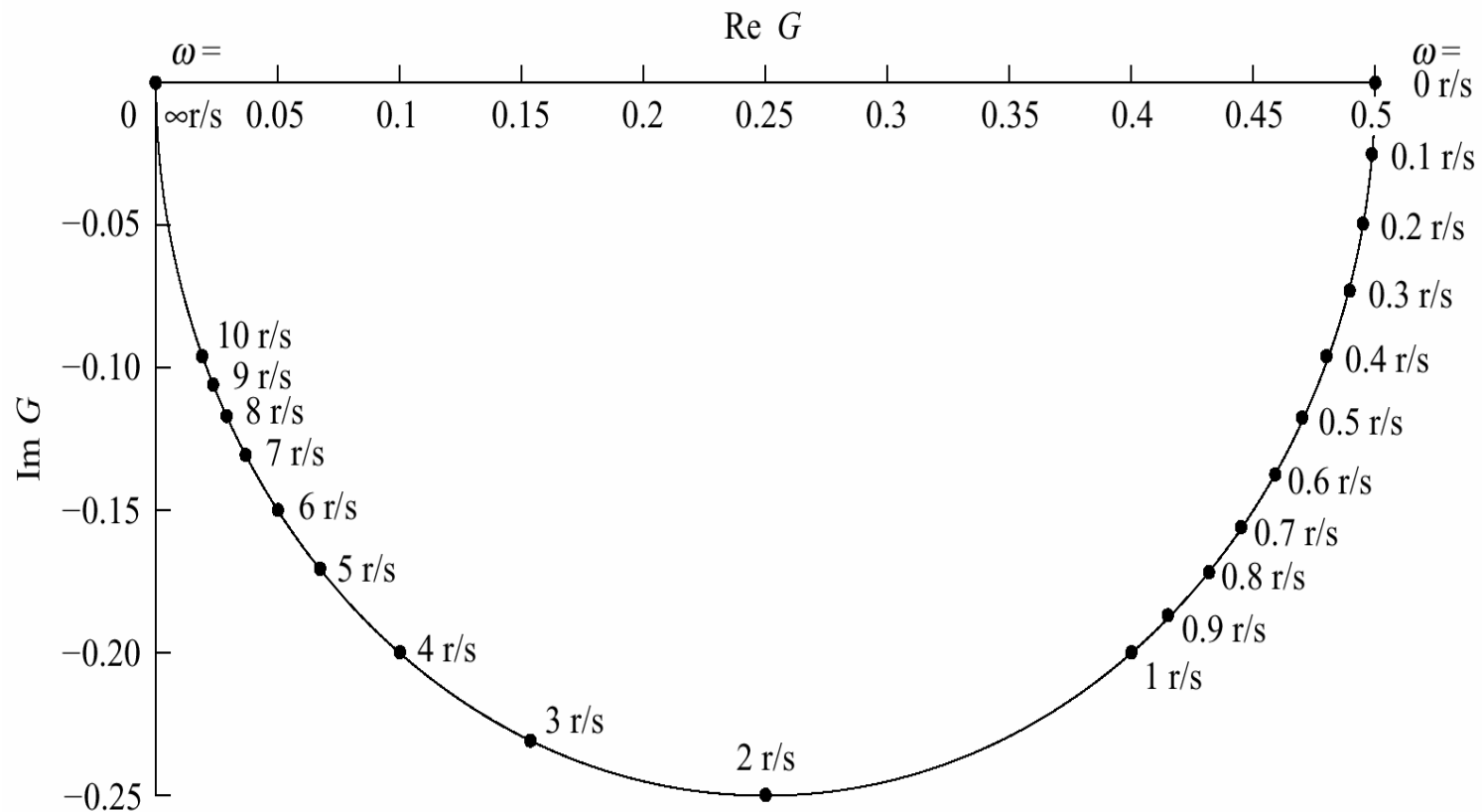
Bode Plot (Magnitude and Phase vs. Frequency)

$$G(s) = 1/(s + 2)$$



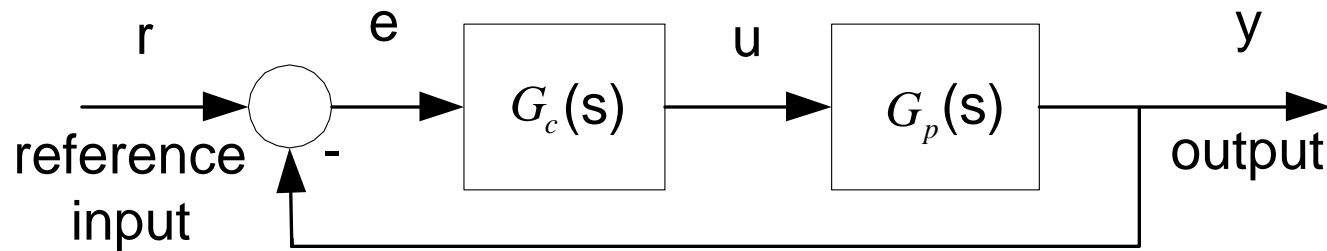
Polar Plot: imaginary part vs. real part of $G(j\omega)$

$$G(s) = 1/(s + 2)$$



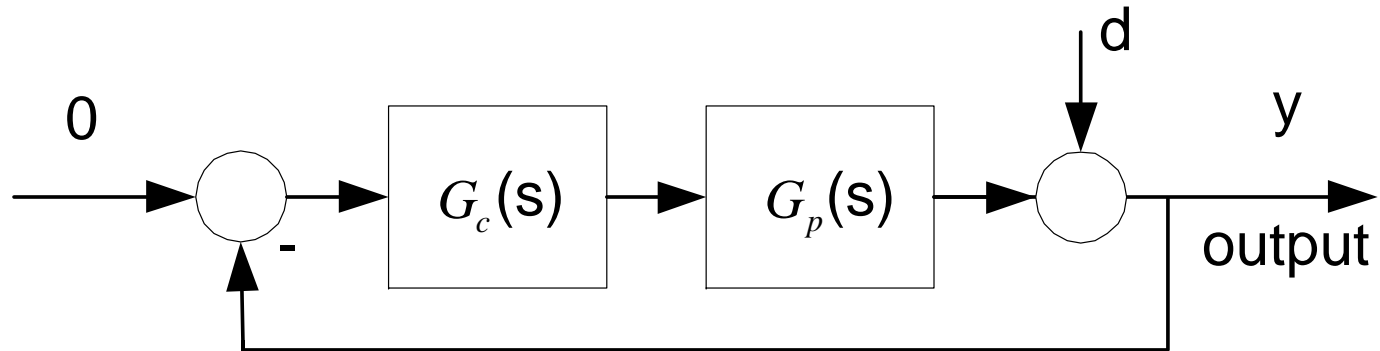
Note: r/s = rad/s

Bandwidth of Feedback Control



- -3dB Frequency of CLTF $\frac{Y(j\omega)}{R(j\omega)} = \frac{G_c(j\omega)G_p(j\omega)}{1 + G_c(j\omega)G_p(j\omega)}$
- 0 dB Crossing Frequency (ω_c) of $G_c(j\omega)G_p(j\omega)$
- Defines how fast y follows r

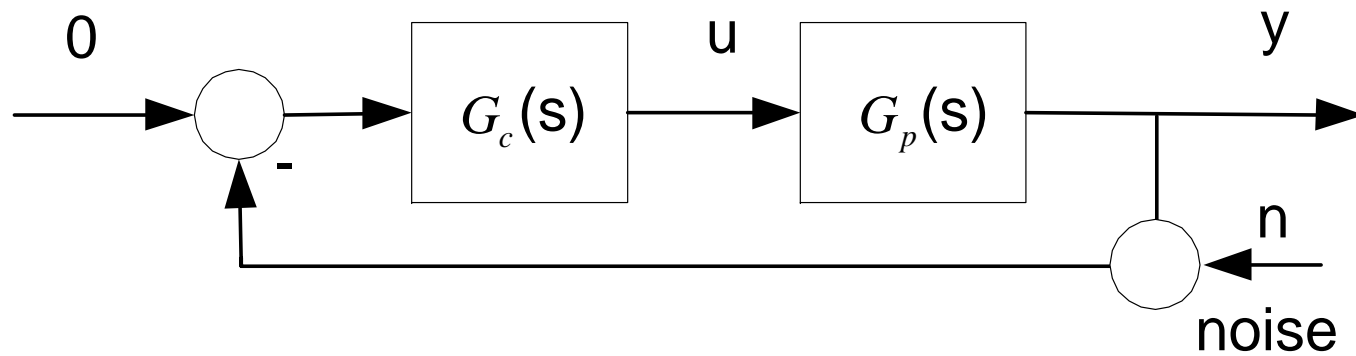
Disturbance Rejection



$$\frac{Y(j\omega)}{D(j\omega)} = \frac{1}{1 + G_c(j\omega)G_p(j\omega)}$$

measures disturbance rejection quality

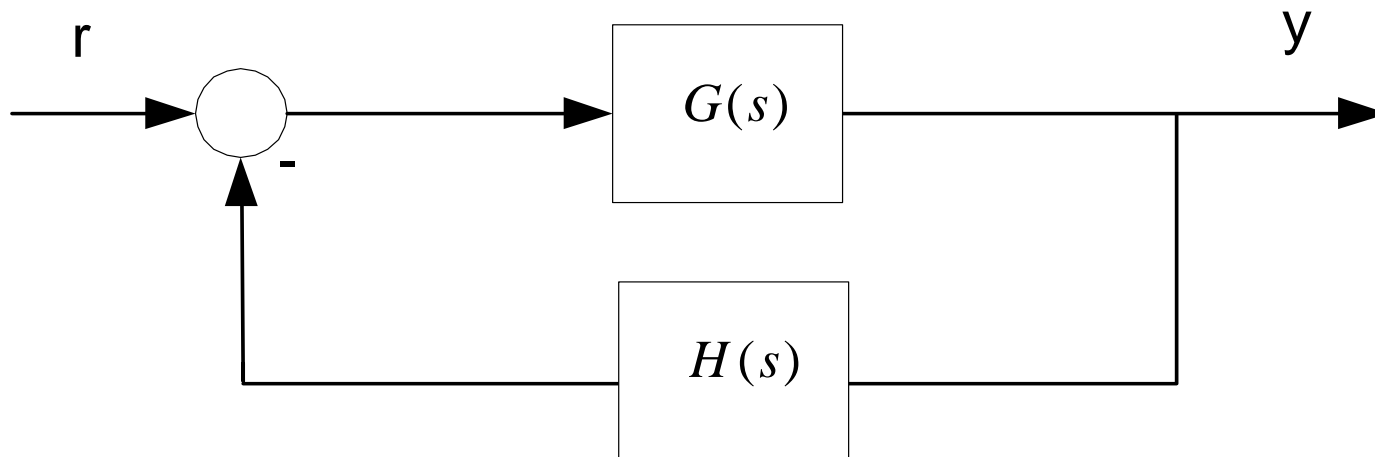
Noise Sensitivity



$$\frac{U(j\omega)}{N(j\omega)} = \frac{-G_c(j\omega)}{1 + G_c(j\omega)G_p(j\omega)}$$
$$\approx -G_c(j\omega) \text{ at high frequency}$$

Nyquist Plot

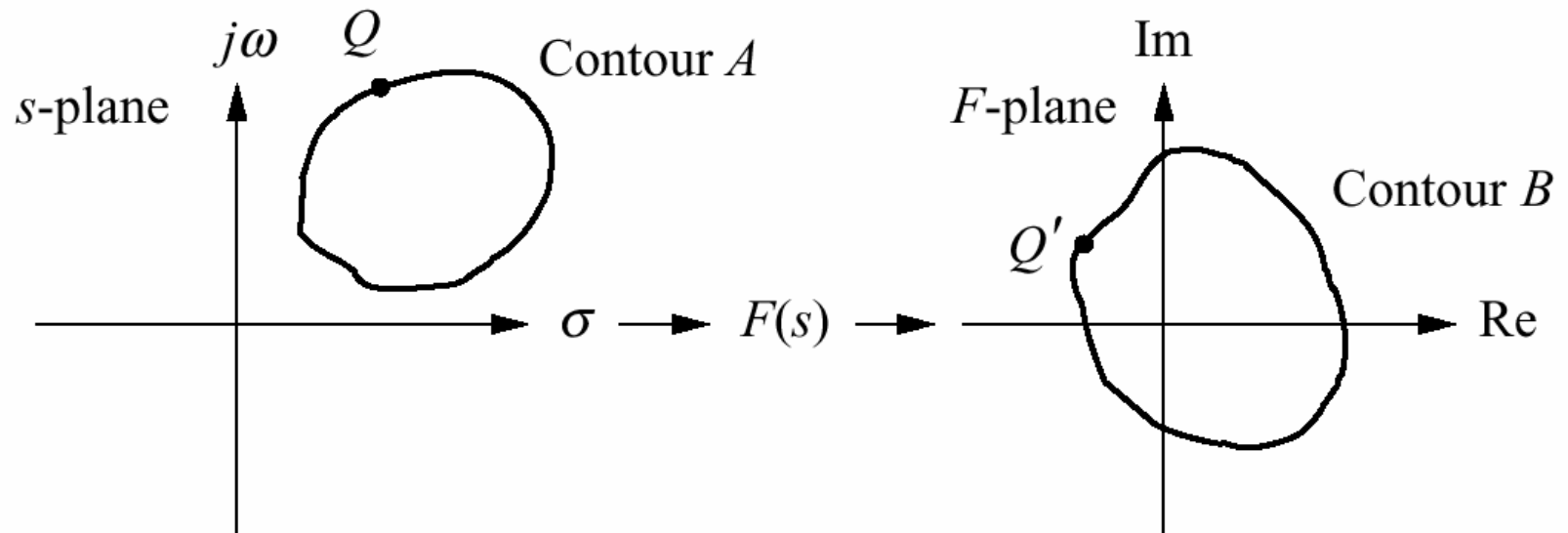
Using $G(j\omega)$ to determine the stability of



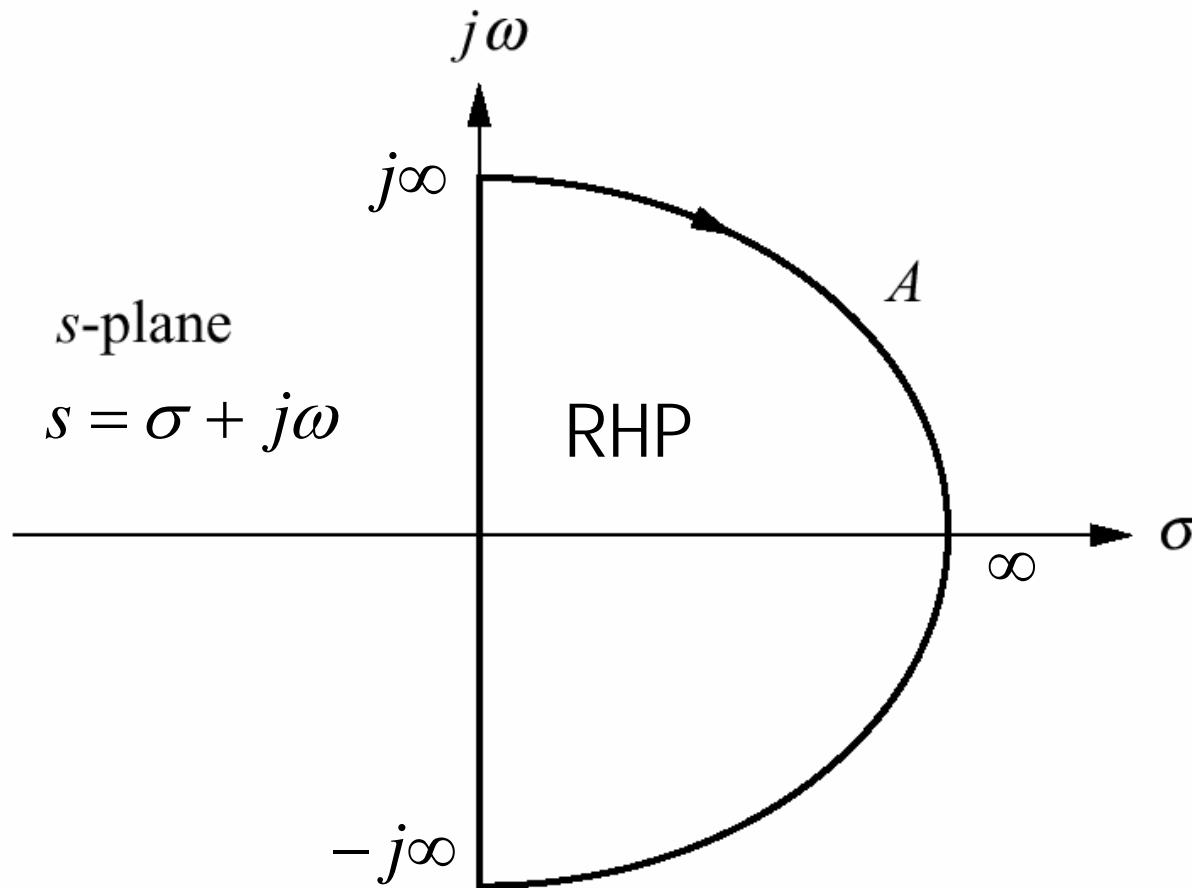
$$G(s) = G_c(s)G_p(s)$$

$H(s)$: Sensor and Filter

The Idea of Mapping



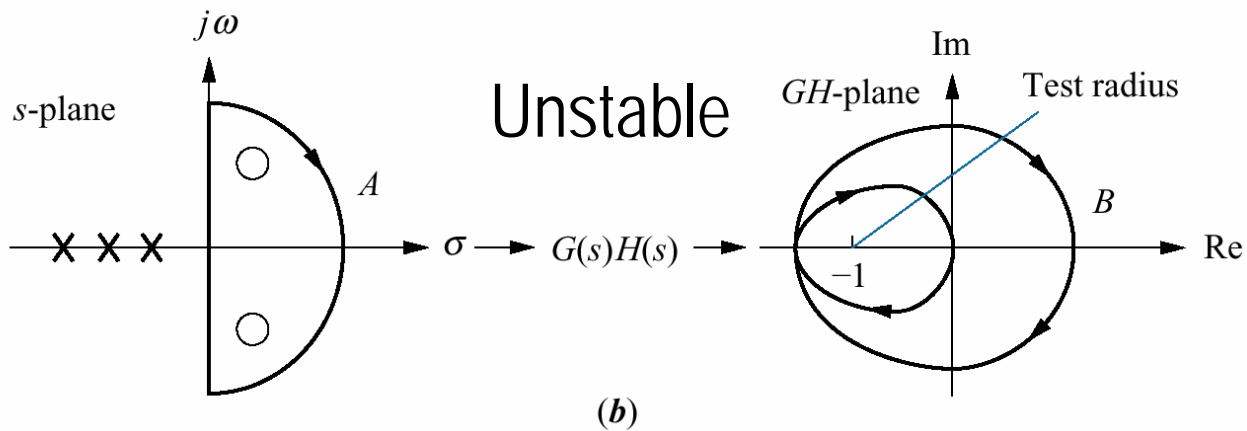
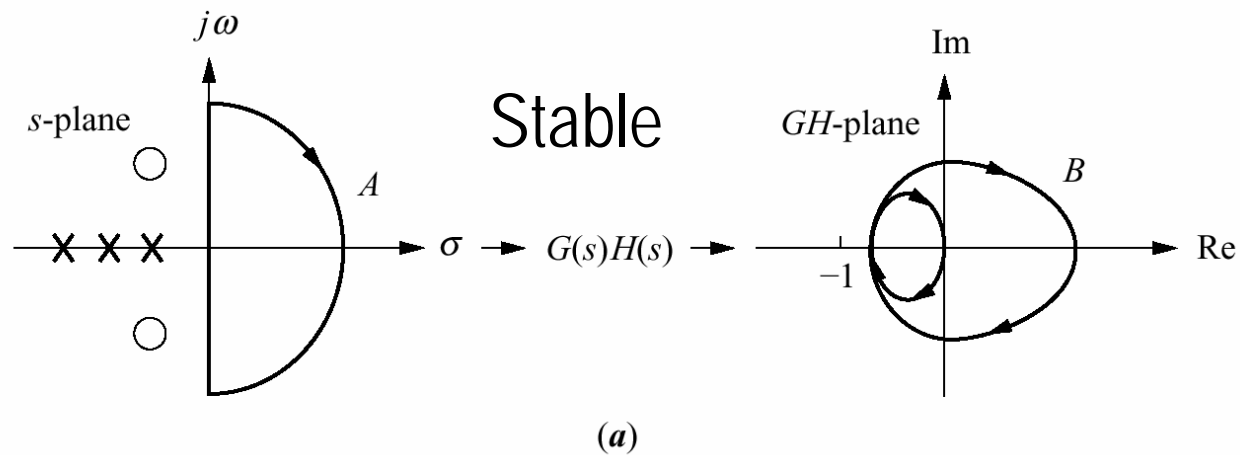
Nyquist Contour



Nyquist Stability Criteria

- Determine stability by inspection
- Assume $G(s)H(s)$ is stable, let s complete the N-countour
 - The closed-loop system is stable if $G(s)H(s)$ does not encircle the $(-1,0)$ point
- Basis of Stability Robustness
- Further Reading: unstable $G(s)H(s)$, # of unstable poles

Nyquist Stability Criteria



○ = zeros of $1 + G(s)H(s)$
 = poles of closed-loop system
 Location not known

× = poles of $1 + G(s)H(s)$
 = poles of $G(s)H(s)$
 Location is known

Stability Robustness

- The (-1,0) point on the GH-plane becomes the focus

- Distance to instability:

$$G(s)H(s) - (-1) = 1 + G(s)H(s)$$

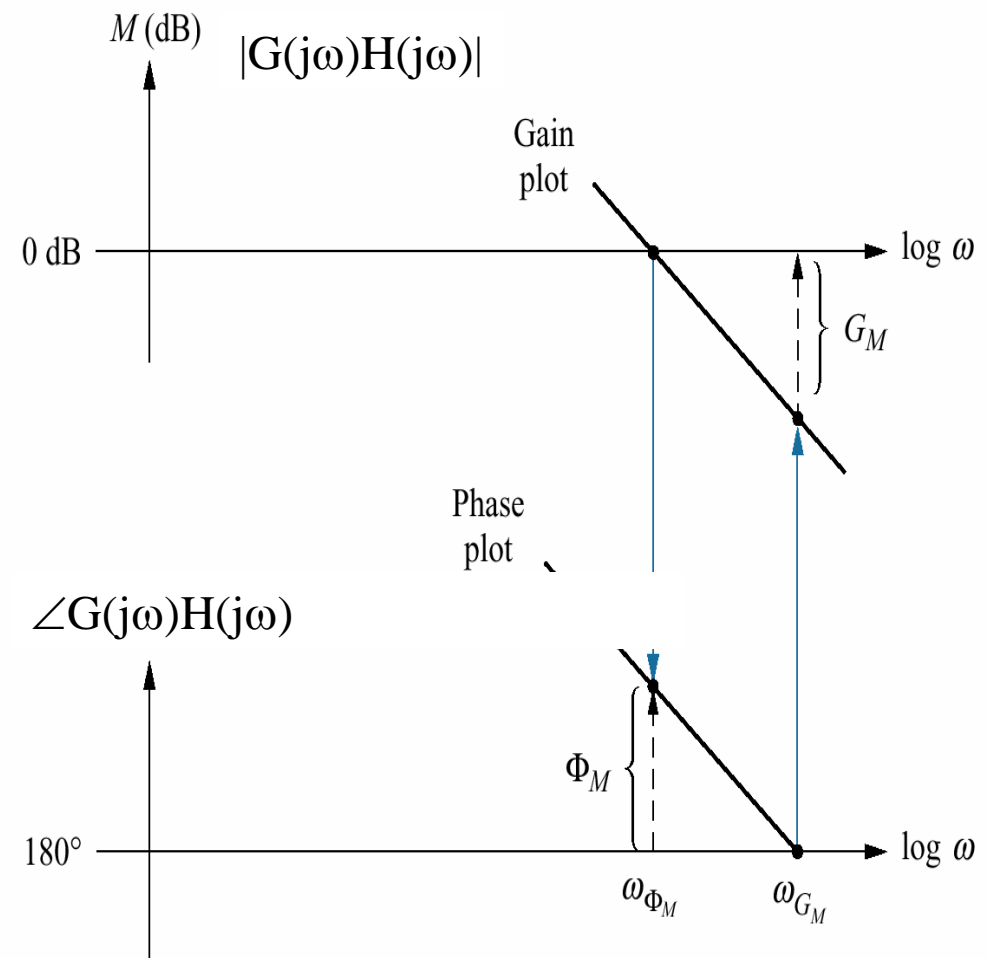
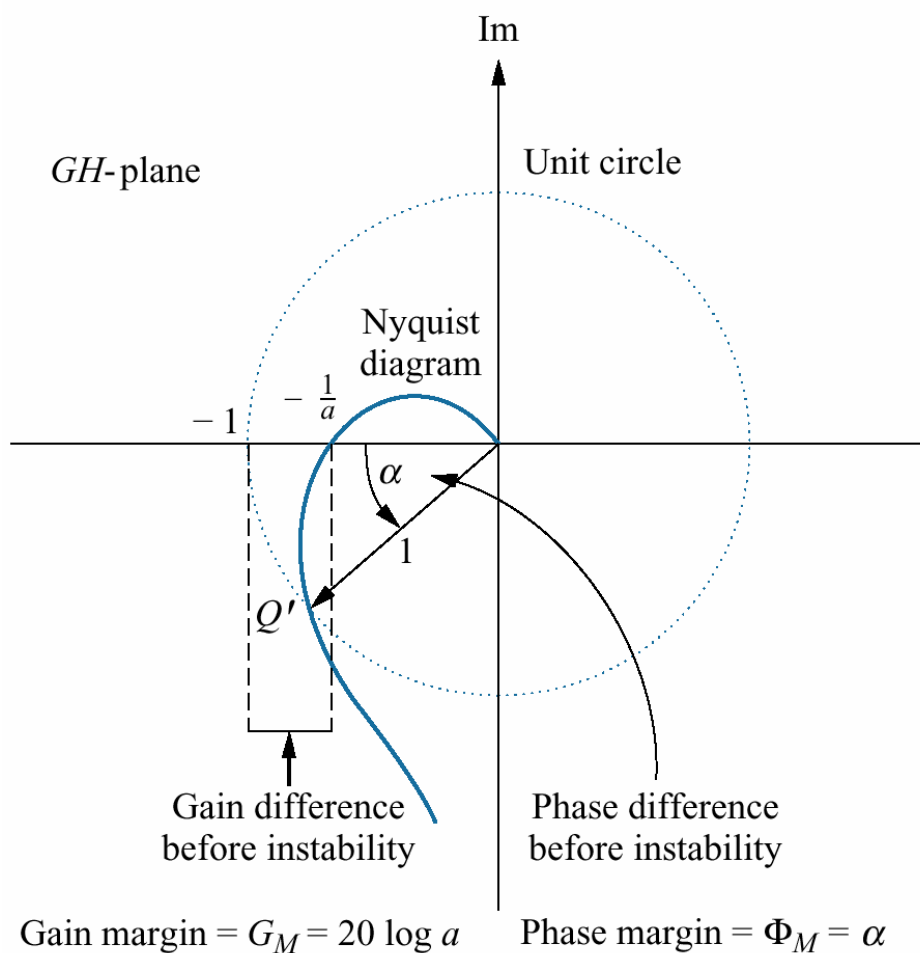
- Robust Stability Condition

Distance to instability > Dynamic Variations of $G(s)H(s)$

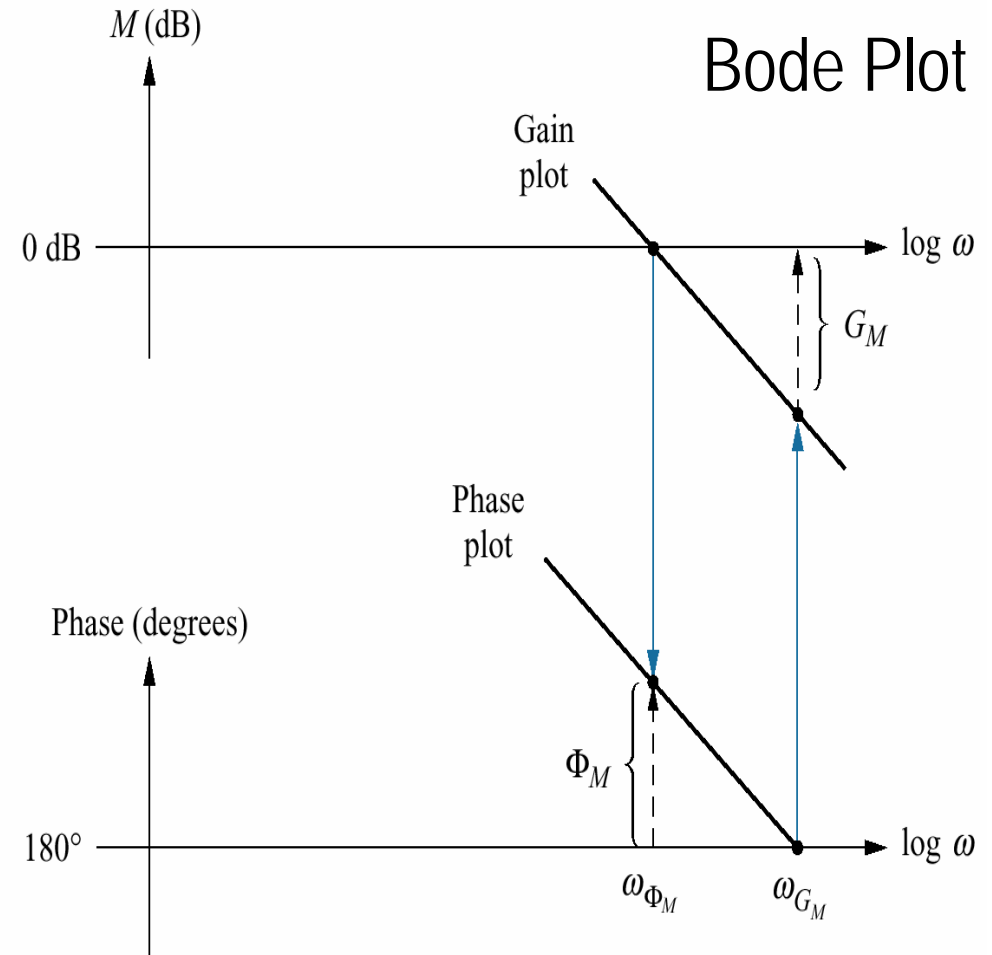
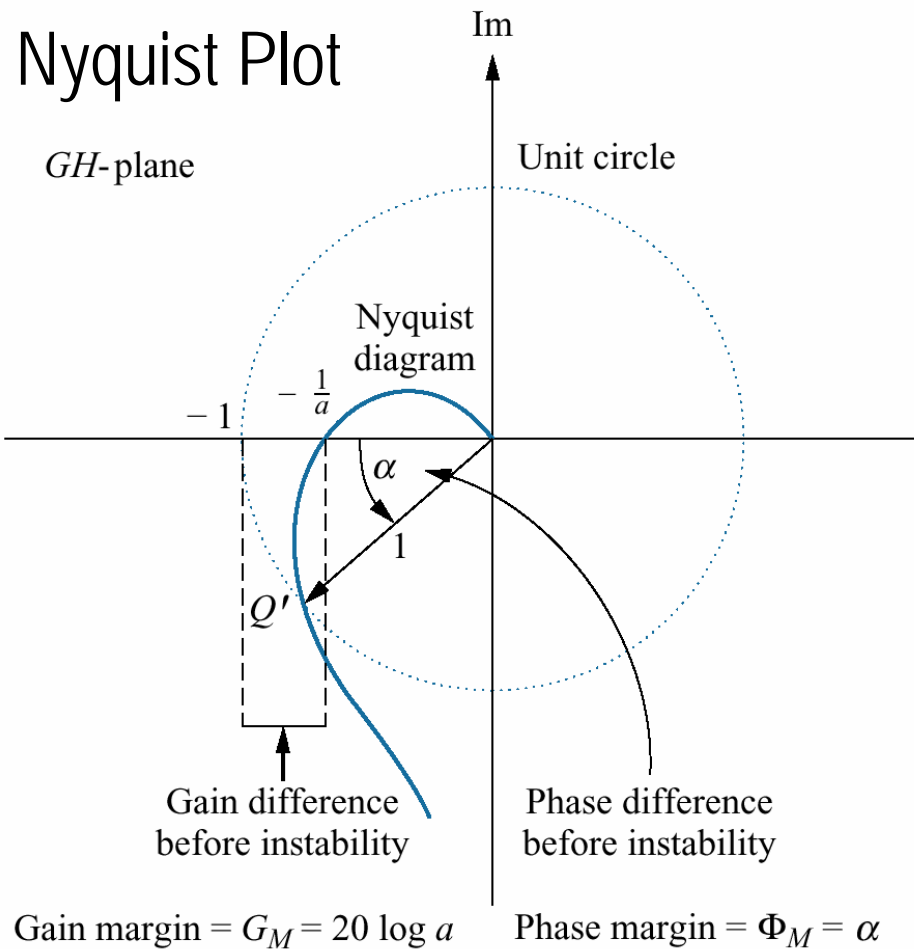
- This is basis of modern robust control theory

Gain and Phase Margins

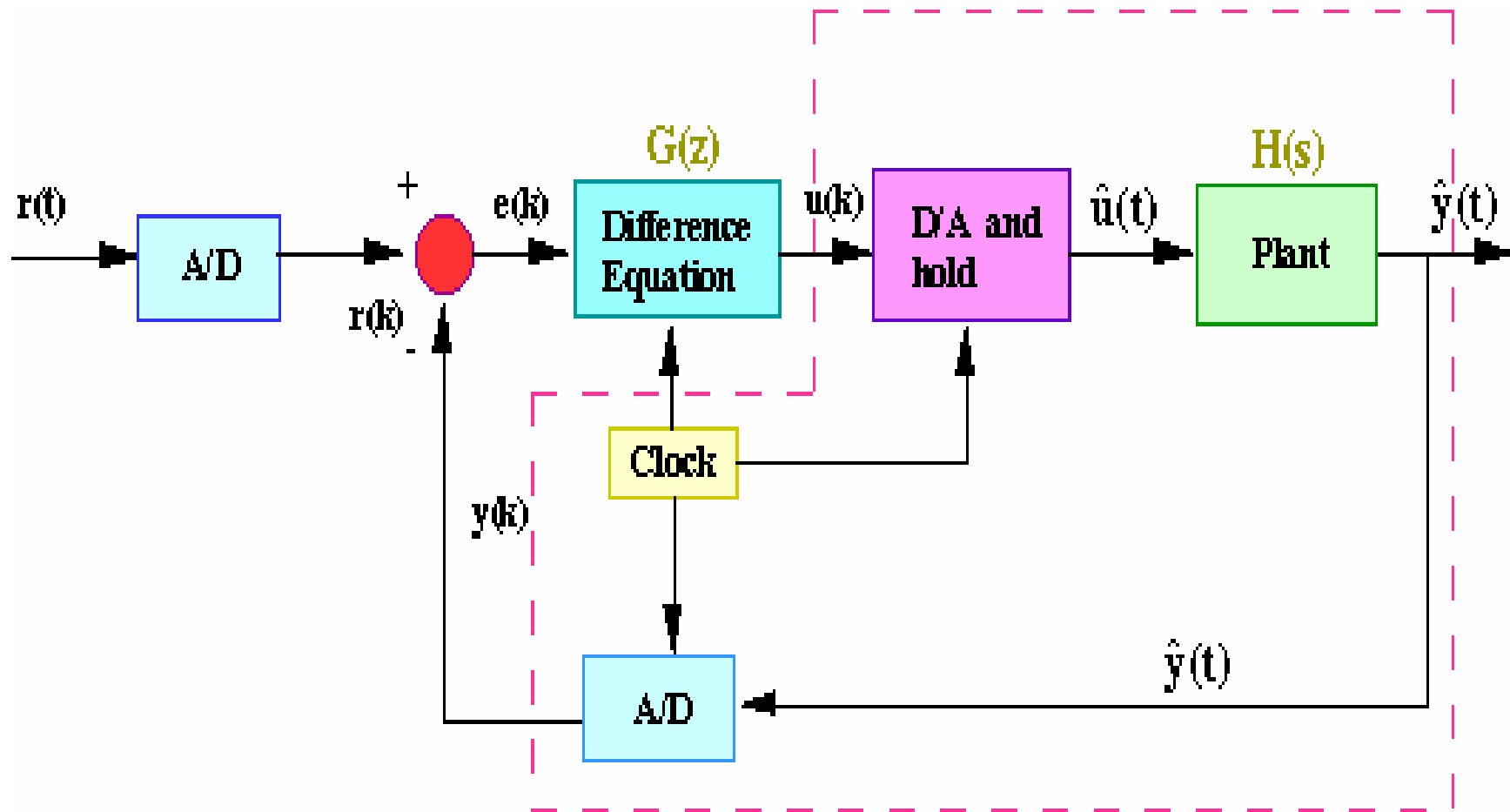
$(-1,0)$ is equivalent of $0\text{db} \angle (-180)^\circ$ point on Bode plot



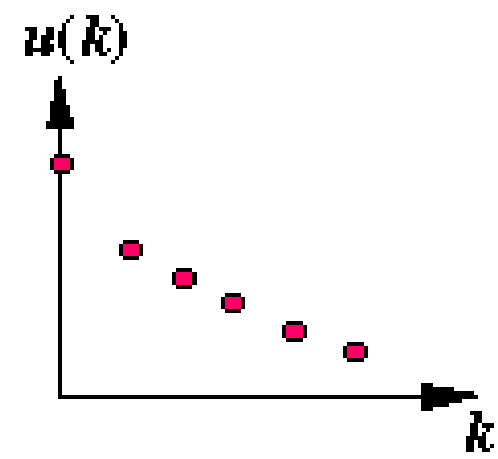
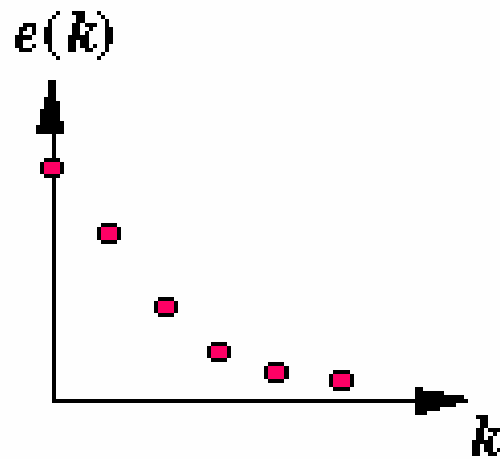
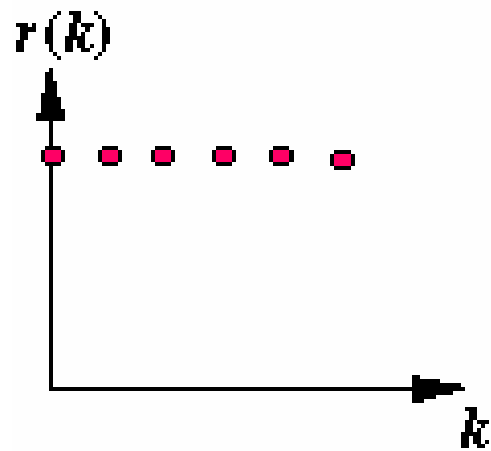
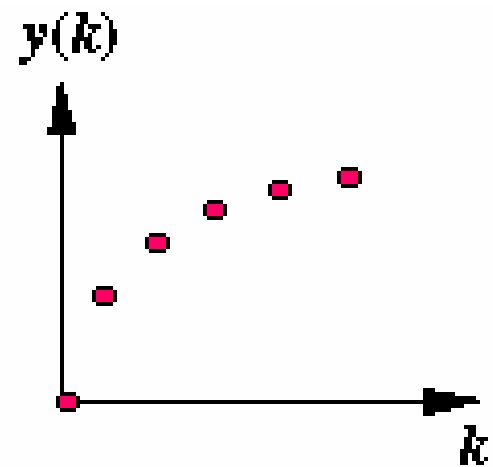
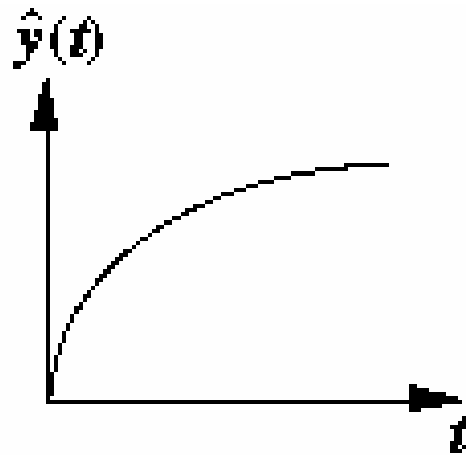
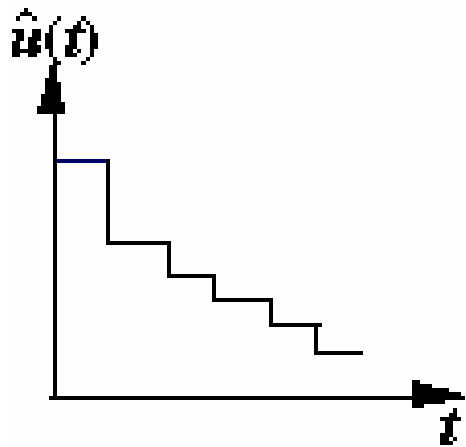
Stability Margins:



Digital Control



Discrete Signals

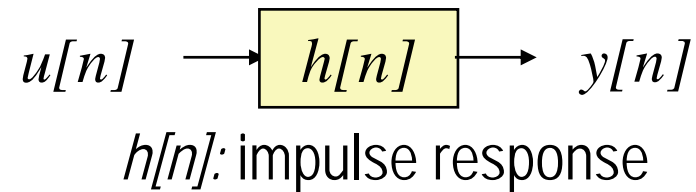


Digital Control Concepts

- Sampling
 - Rate
 - Delay
- ADC and DAC
 - Resolution (quantization levels)
 - Speed
 - Aliasing
- Digital Control Algorithm
 - Difference equation

Discrete System Description

- Discrete system



- Difference equation

$$\sum_{k=0}^N a_k y[n-k] = \sum_{k=0}^M b_k u[n-k]$$

Discrete Fourier Transform and z-Transform

$$X(e^{j\omega}) = \sum_{n=-\infty}^{\infty} x[n]e^{-j\omega n}$$

$$X(z) = \sum_{n=-\infty}^{\infty} x[n]z^{-n}$$

Discrete Transfer Function and Frequency Response

$$H(z) = \frac{Y(z)}{X(z)} = \frac{\sum_{k=0}^M b_k z^{-k}}{\sum_{k=0}^N a_k z^{-k}}$$

$$H(e^{j\omega}) = H(z)|_{z=e^{j\omega}}$$

Application of Basic Concepts to Previously Designed Controllers